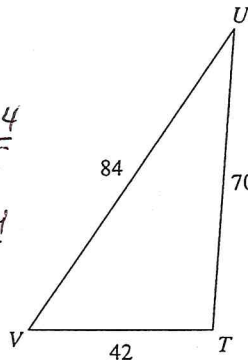


7)

$$\frac{84}{30} = \frac{14}{5}$$

$$\frac{70}{25} = \frac{14}{5}$$

$$\frac{42}{15} = \frac{14}{5}$$



Because

$$\frac{TU}{QR} = \frac{TV}{RS} = \frac{VT}{SQ} = \frac{14}{5}$$

corresponding sides are proportional.

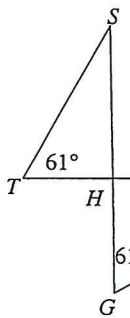
Therefore,

$$\Delta TUV \sim \Delta QRS$$

by SSS ~.

$$\Delta TUV \sim \Delta QRS$$

9)

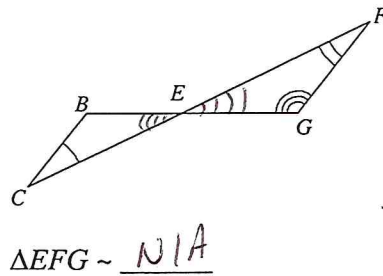


$\angle G \cong \angle T$ by given and
 $\angle SHT \cong \angle FHG$ because
 vertical $\angle$'s are $\cong$. Therefore

$\Delta SHT \sim \Delta FHG$ by
 AA ~

$$\Delta HGF \sim \Delta HST$$

8)

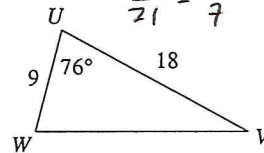


$$\Delta EFG \sim \Delta NIA$$

Although vertical
 $\angle$'s are $\cong$, one
 $\cong$ pair is not
 enough to
 prove ~.

$$\frac{18}{42} = \frac{3}{7}$$

$$\frac{9}{21} = \frac{3}{7}$$

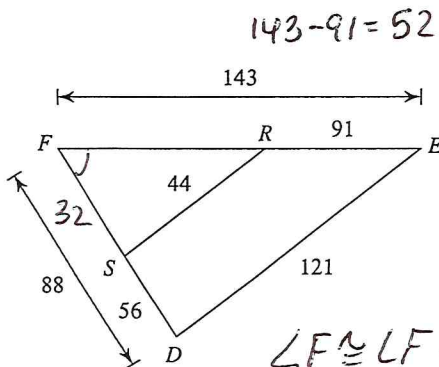


Since $\frac{UW}{FH} = \frac{WV}{FG} = \frac{3}{7}$,
 surrounding sides
 are proportional.
 the included $\angle$'s
 are $\cong$, $\angle U \cong \angle F$
 because they both
 have measure
 76°. The Δ 's are
 ~ by SAS ~.

$$\Delta FGH \sim \Delta UWV$$

$$\Delta FGH \sim \Delta UWV$$

11)



$$\frac{88-56}{143-91} = \frac{32}{52}$$

$$\Delta FED \sim \Delta FRS$$

$\angle F \cong \angle F$ by reflexive PC
 and the sides surrounding
 it have the same
 ratio $\frac{FS}{FD} = \frac{FR}{FE} = \frac{4}{11}$.

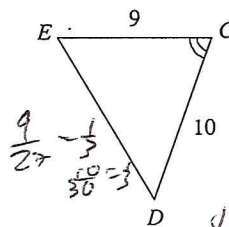
Therefore, $\Delta FED \sim \Delta FRS$
 by SAS ~

$$\frac{32}{88} = \frac{4}{11}$$

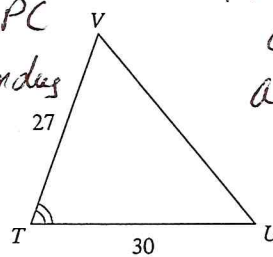
$$\frac{52}{143} = \frac{4}{11}$$

(÷18)

12)



$$\frac{9}{27} = \frac{1}{3}$$



$$\Delta TUV \sim \Delta CDE$$

$\angle C \cong \angle T$ by given, and
 the surrounding
 corresponding sides
 are in proportion

$$\frac{CE}{TV} = \frac{CD}{TU} = \frac{1}{3}$$

Therefore,
 $\Delta TUV \sim \Delta CDE$
 by SAS ~